

# High temperature stability of MGC gas turbine components in combustion gas flow environments

**Narihito NAKAGAWA**, Hideki OHTSUBO, Kazutoshi SHIMIZU,  
Atsuyuki MITANI, Kohji SHIBATA  
Ube Research Laboratory, Corporate Research and Development  
UBE INDUSTRIES, LTD.

Yoshiharu WAKU:  
High Performance Gas Turbine Research Association  
**EUROMAT 2005**  
**5 –8 September 2005**  
**Prague, Czech Republic**

# Contents

---

## **1. The characteristics of the binary MGCs:**

- (1) Background & motivations
- (2) Fabrication process
- (3) Microstructures
- (4) Thermal stability of microstructures and strength
- (5) Mechanism of high temperature characteristics

## **2. Outline and Current Research Topics in National Project (NEDO):**

- (1) Final targets of MGCs applied gas turbine system
- (2) High-temperature stability of the trial components
- (3) Possibility of low-cost process technology by near-net shape casting
- (4) Basic exposure test in combustion gas flow environment

## **3. Improvement of high-temperature strength characteristics:**

- (1) The refinement of the binary MGCs microstructure
- (2) Introduce of recently developed the new ternary MGC

## **4. Another applications to making use of composition and properties MGCs**

# Background

## 1. Global warming prevention & Energy-saving

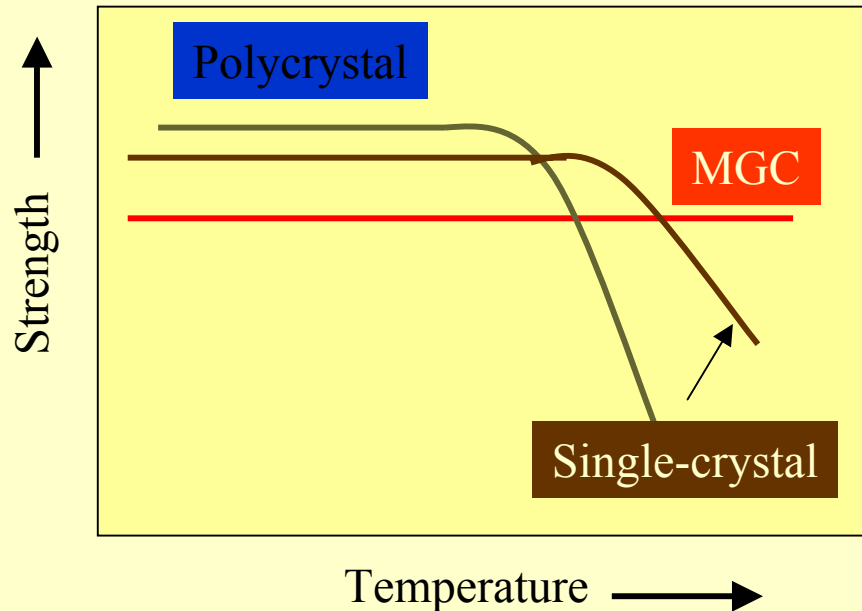
## 2. Thermal efficiency improvement;

Develop high-performance structural materials

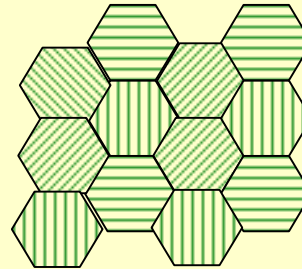
→ Stable remain at 1500 °C or higher in air

→ improvement of microstructure oxide

MGC's microstructure have superior high temperature strength that overcome polycrystal and single-crystal materials.



## Polycrystal

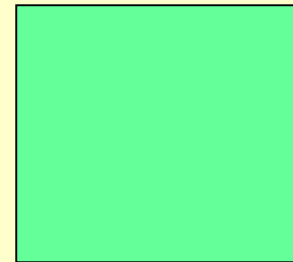


- Micro grain superplasticity due to grain-boundary sliding or rotation at high temperature



- Remarkable decrease of high temperature strength of oxide ceramics

## Single-crystal



- No barrier (interface) to disturb dislocation motion



- Gradual decrease of high temperature strength

## MGC



- No grain-boundary sliding or rotation ( against polycrystal)
- Interface prevent dislocation motion ( against single-crystal)



- Excellent high temperature strength

# Fabrication Process

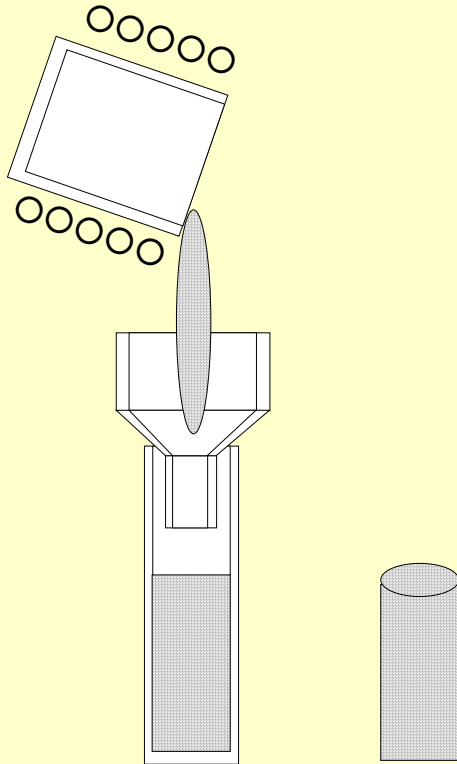
Commercially available  $\text{Al}_2\text{O}_3$  powder and  $\text{Y}_2\text{O}_3$  powder or  $\text{Gd}_2\text{O}_3$  powder were mixed for the mole ratio of eutectic composition. Preliminary melting is performed by high-frequency induction heating and casted into to a molybdenum crucible to obtain an ingot. Unidirectionally solidification was carried out by using the Bridgman type furnace.

○  $\text{Al}_2\text{O}_3/\text{YAG}$  :

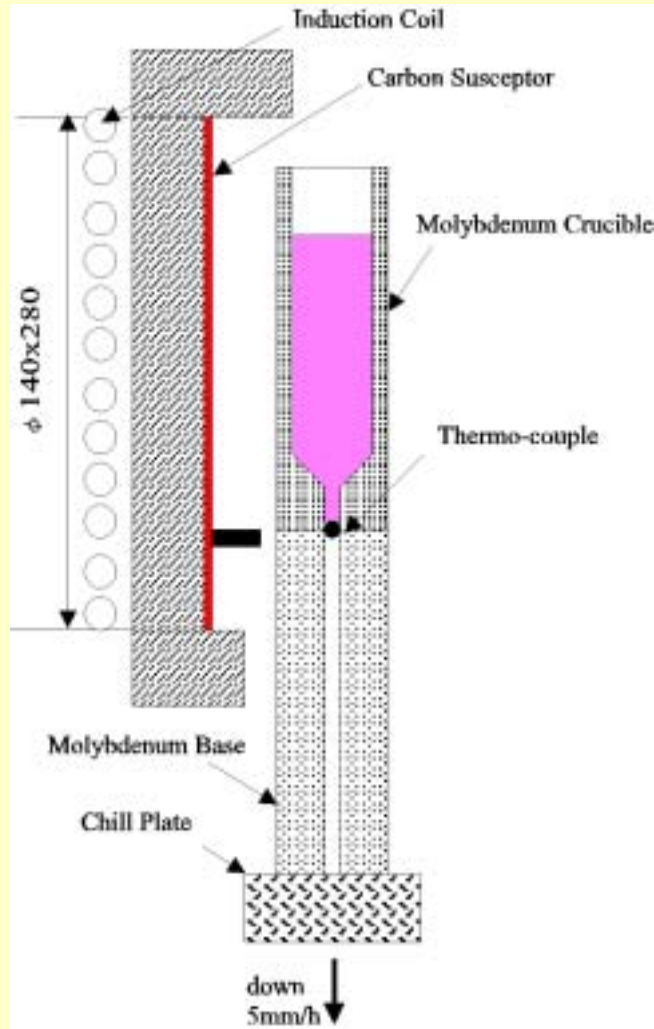
$\text{Al}_2\text{O}_3/\text{Y}_2\text{O}_3 = 82/18$  mole % ratio

○  $\text{Al}_2\text{O}_3/\text{GAP}$  :

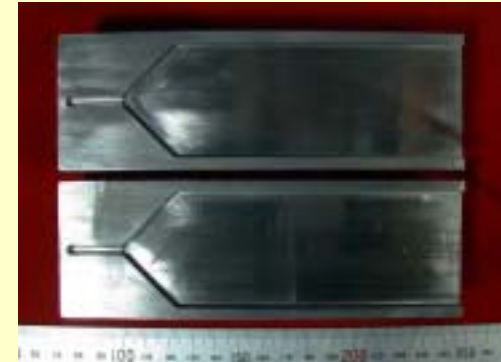
$\text{Al}_2\text{O}_3/\text{Gd}_2\text{O}_3 = 78/22$  mole % ratio



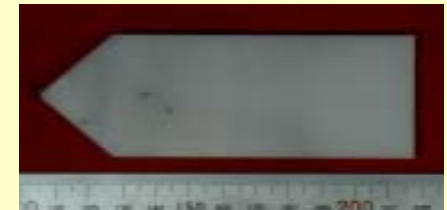
Ingot making



Unidirectional Solidification



Molybdenum divided mold



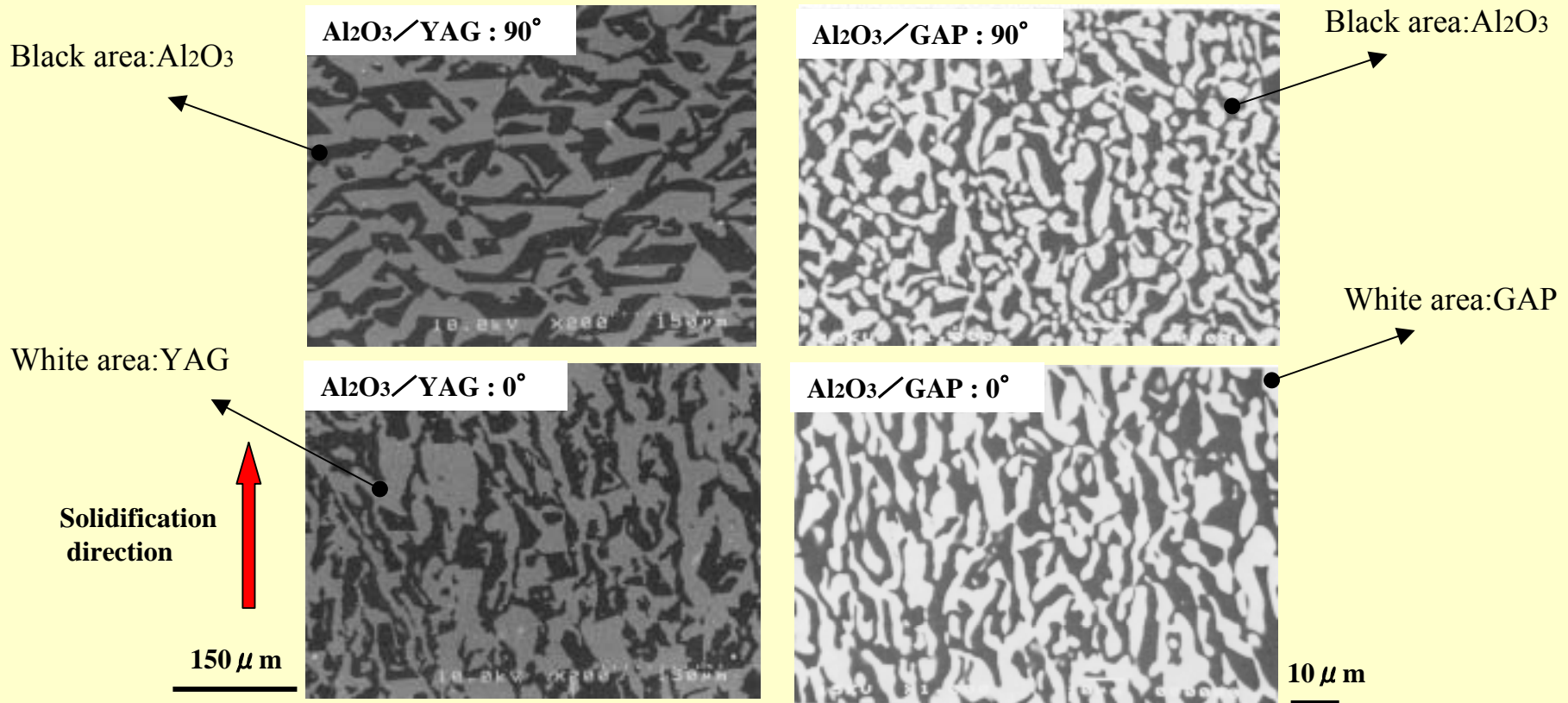
$\text{Al}_2\text{O}_3/\text{YAG}$  plate (45\*90\*6)



$\text{Al}_2\text{O}_3/\text{GAP}$  rod ( $\Phi 53$  mm)

# Microstructures

The MGC materials have new microstructures, which are composed of continuous network of single-crystal  $\text{Al}_2\text{O}_3$  phases and single-crystal oxide compounds ( YAG, GAP ) without grain boundaries.

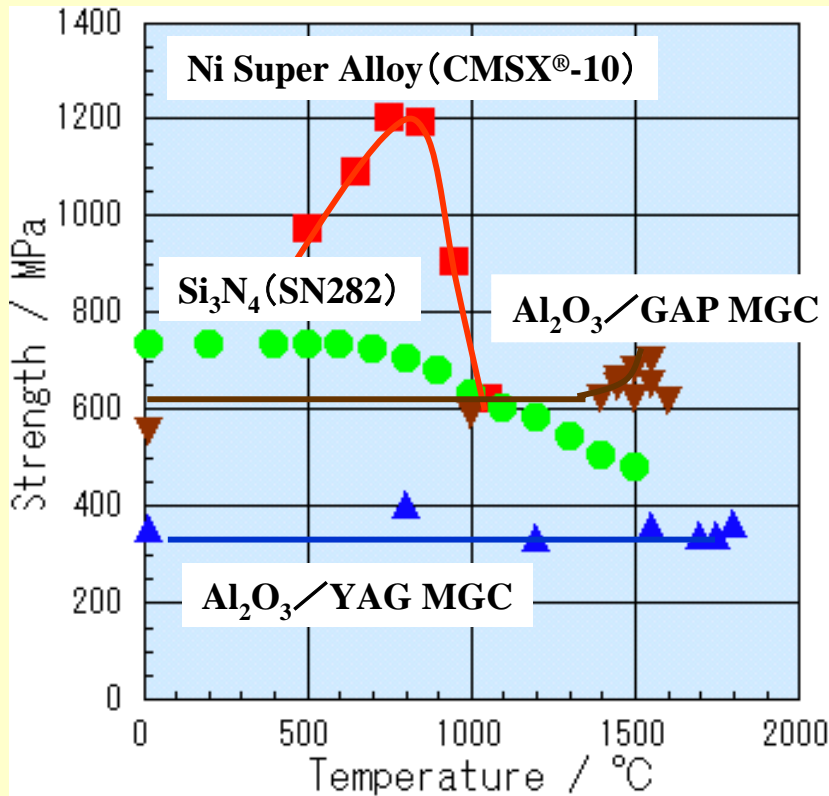


SEM images of the microstructures of cross section perpendicular (  $90^\circ$  direction ) and parallel (  $0^\circ$  direction ) to the solidification direction of the MGC materials.

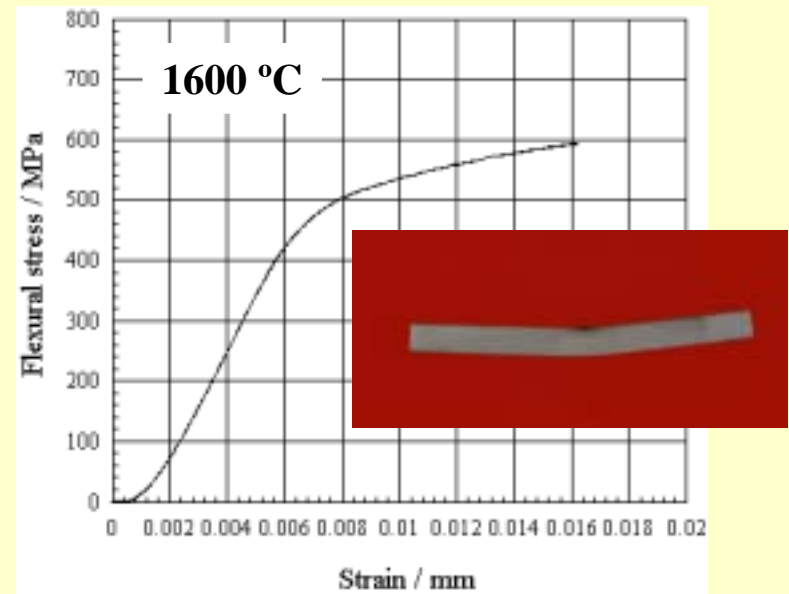
$\text{Y}_3\text{Al}_5\text{O}_{12}$  ( YAG : Yttrium Aluminum Garnet ) ,  $\text{GdAlO}_3$  ( GAP : Gadolinium-Aluminum-Perovskite )

# High Temperature Strength Characteristics

The  $\text{Al}_2\text{O}_3/\text{YAG}$  binary MGC maintains its room temperature strength up to about  $1700^\circ\text{C}$ , with flexural strength in the range of 300 - 350 MPa. The  $\text{Al}_2\text{O}_3/\text{GAP}$  binary MGC shows approximately 600 MPa from  $1400^\circ\text{C}$  to  $1600^\circ\text{C}$ . Ni-based superalloys shows a large drop in strength above around  $800^\circ\text{C}$ . And  $\text{Si}_3\text{N}_4$  has the higher than the  $\text{Al}_2\text{O}_3/\text{GAP}$  MGC, but its strength decreases gradually above  $800^\circ\text{C}$ .



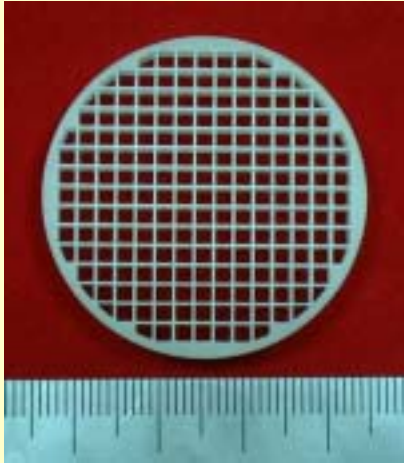
The  $\text{Al}_2\text{O}_3/\text{GAP}$  MGC shows yielding behavior under high stress above  $1600^\circ\text{C}$ , with a flexural yield stress of around 600MPa.



Temperature dependence of the strength in representative high temperature structural material.  
\*Ni super alloy: Tensile strength

Typical stress-displacement curve of the 4-point flexural test of  $\text{Al}_2\text{O}_3/\text{GAP}$  MGC at  $1600^\circ\text{C}$ .

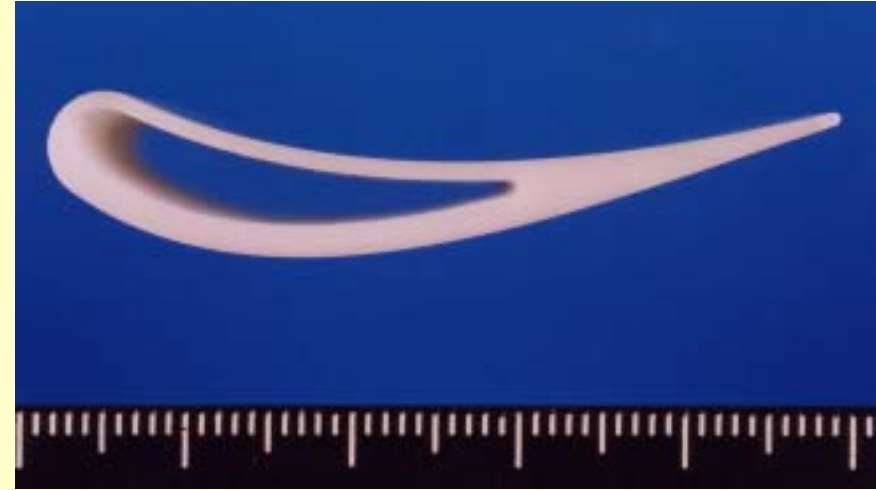
# Machinability



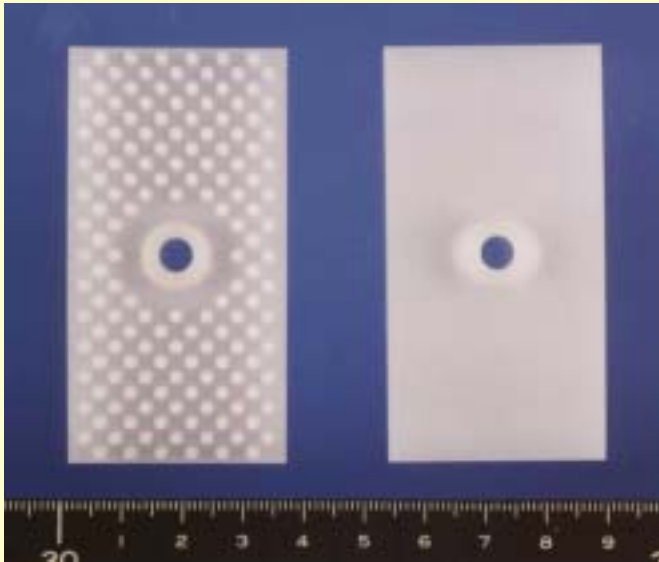
Filter



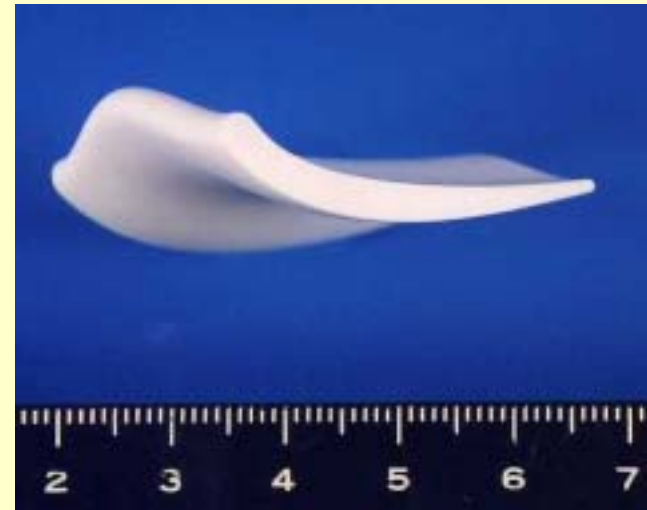
Volts



Hollow type turbine nozzle vane



Heat shield panels of combustion liner



Bowed stacked turbine nozzle vane

# Motivations

---

## 1. Directionally Solidified Eutectic Ceramics;

- \* Improve the microstructure and the mechanical properties using unidirectional solidification  
ex. Binary System;  $\text{Al}_2\text{O}_3/\text{Y}_3\text{Al}_5\text{O}_{12}$ (YAG),  $\text{Al}_2\text{O}_3/\text{GdAlO}_3$ (GAP),  $\text{Al}_2\text{O}_3/\text{Er}_3\text{Al}_5\text{O}_{12}$ (EAG)  
Ternary System;  $\text{Al}_2\text{O}_3/\text{Y}_3\text{Al}_5\text{O}_{12}$ (YAG)/ $\text{ZrO}_2$  ,  $\text{Al}_2\text{O}_3/\text{Er}_3\text{Al}_5\text{O}_{12}$ (EAG)/ $\text{ZrO}_2$

## 2. MGC's Advantages;

- \* High mechanical strength up to melting point temperature
- \* High creep resistance and oxidation resistances
- \* Good machinability and productivity to fabricate complex shape components

**NEDO Project ( FY2001-05 )**  
**Research and Development on**  
**MGC Applied Gas Turbine System**

Basic technologies to apply the high temperature section for a gas turbine

- \* System Integration Technology : IHI & KHI
- \* **Materials & Process Technology : UBE**

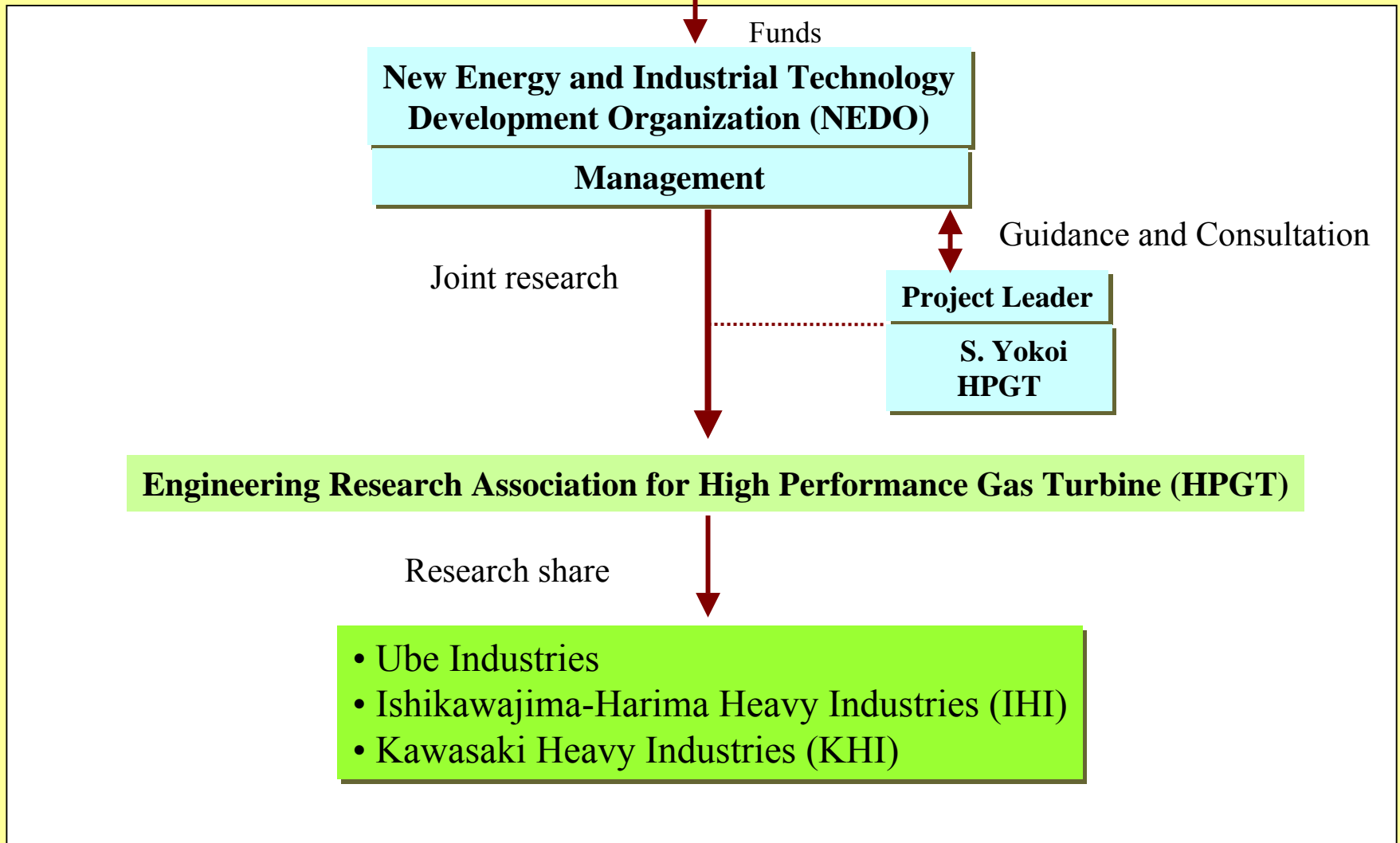


# Implementation

*Project term*  
*FY2001-2005*

Ministry of Economy, Trade and Industry (METI)

*Budget (FY2004)*  
*33 million yen*



# Outline of Research and Development on Processing Technology for Superior Heat-Resistant Melt Growth Composites (MGC)

## Processing Technology

### R&D on Innovative Process & Manufacturing Technology

1. Near-net shape casting of complex shape components
2. Improvements of materials reliability & long-term durability under severe Environments (highly water vapor Pressurized at ultra-high temperature)
3. MGC's application technology to the high temperature section of the gas turbine system

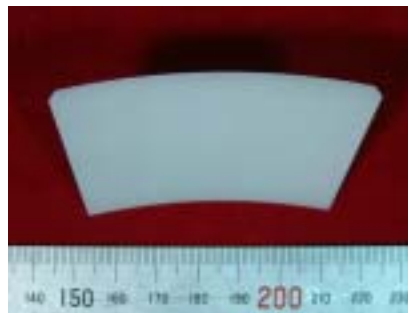
### Goals

- Development of near-net shape casting technology
- Thermal stability:  $\sim 1,700\text{ }^{\circ}\text{C}$

## Application Technology to the hot section of the gas turbine

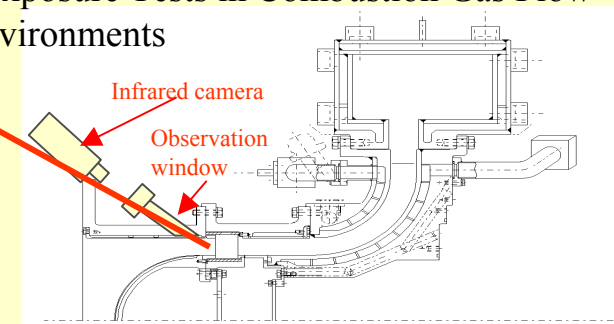


MGC turbine nozzle vane

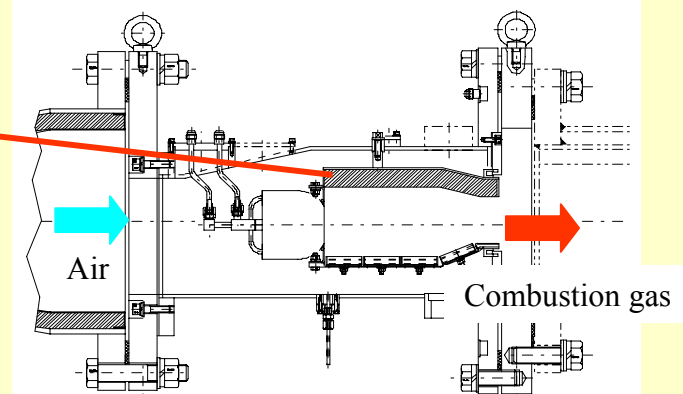


MGC heat shield panel for Combustor liner

- Improving Design Technology
- Exposure Tests in Combustion Gas Flow Environments



Cross-section drawing of the high temperature nozzle rig

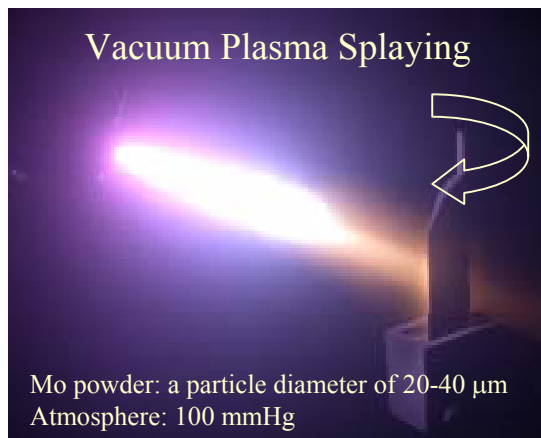


1/4 sector combustor rig

# 1. Fabrication process of plasma sprayed quasi-turbine nozzle mold for near-net shape casting for MGC components



Quasi-turbine nozzle copper model



Thickness of wall of mold: 2-3 mm



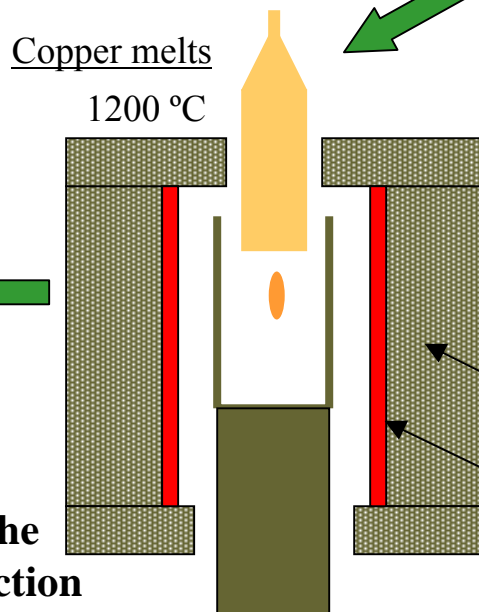
A plasma sprayed mold on a quasi-turbine nozzle copper model



Al<sub>2</sub>O<sub>3</sub>/GAP sample



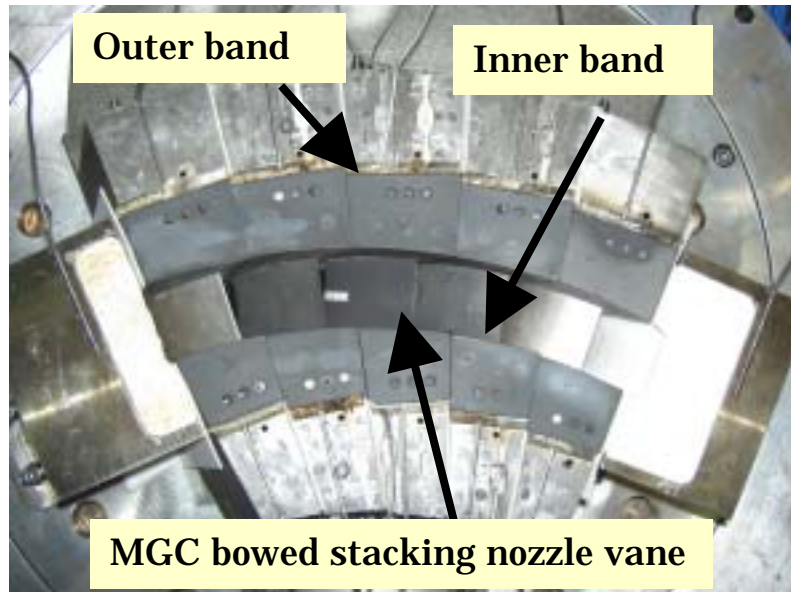
Cross-section diagram of the plasma sprayed mold at the middle of the longitudinal direction



## 2. MGC turbine nozzle test rig

The high temperature nozzle rig ( maximum temperature  $\sim 1700^{\circ}\text{C}$ ) have been improved to measure continuous temperature distribution on the nozzle surface by using an infrared camera.

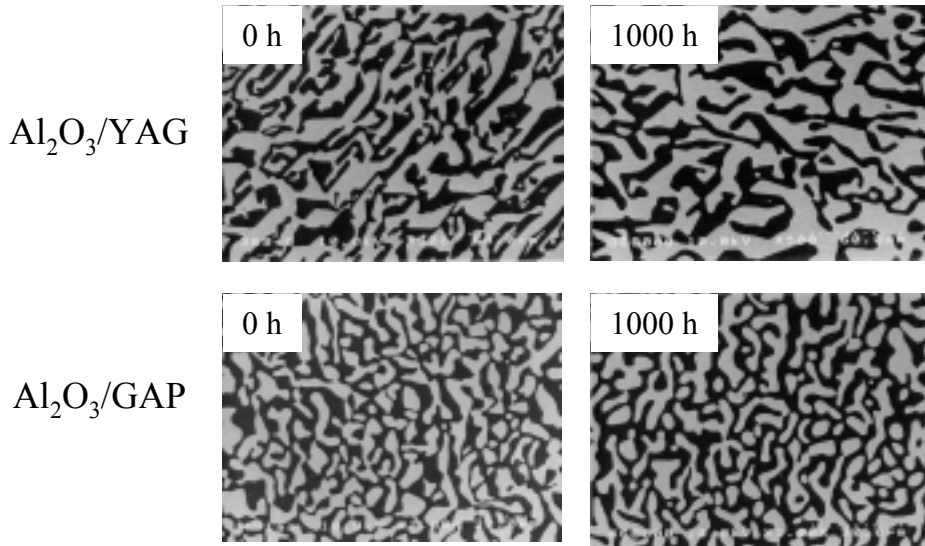
We are now planning the test rig at an inlet gas temperature level of  $1700^{\circ}\text{C}$  in order to ensure the structural integrity under the steady-state and thermal shock conditions.



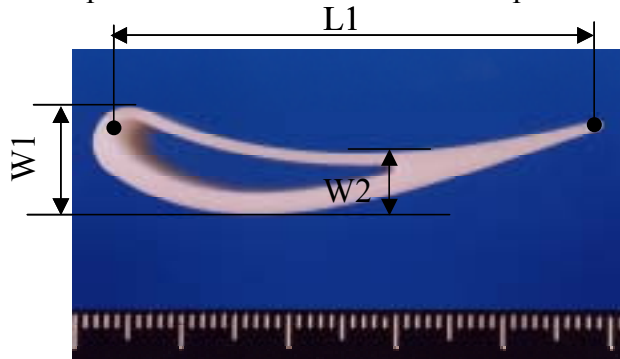
- Completed successfully  $1500^{\circ}\text{C}$  steady-state condition test
- Confirmed no damage in MGC nozzle vane and MGC heat shield panel

# Thermal Stability of MGC Components

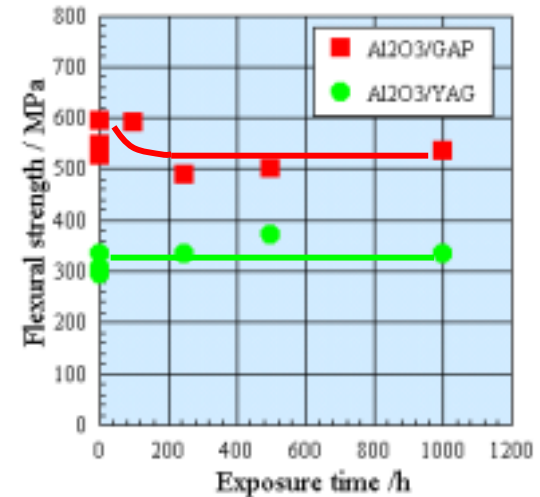
Even after 1000 hours of exposure test at 1700 °C in an air atmosphere, no grain growth was observed in the microstructures. The MGC components have excellent oxidation resistance with no change in weight and surface roughness after 1000 hour at 1700 °C in an air atmosphere.



SEM images of the microstructures of MGC after 1000 hours of exposure at 1700 °C in an air atmosphere.



Hollow turbine nozzle vane



Relationship between 4 point flexural strength at room temperature and time of heat treatment at 1700 °C in air.

Table.1 Difference of the MGC nozzle vane after exposure test for 1000 hours at 1700 °C in an air atmosphere.

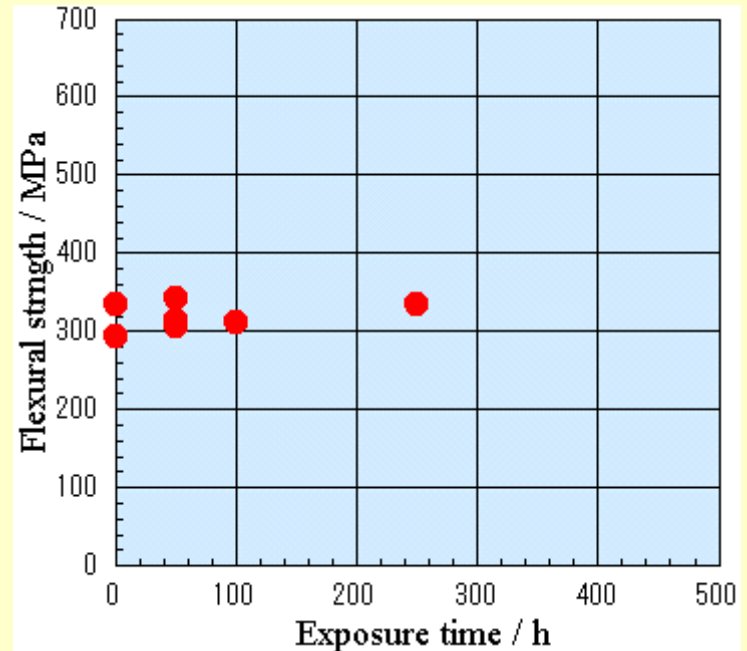
Length	0 h	500 h	1000 h	Dimensional change
L1 (mm)	43. 971	43. 977	44. 000	0. 029
W1 (mm)	10. 614	10. 614	10. 598	-0. 022
W2 (mm)	5. 389	5. 385	5. 371	-0. 019
Weight (g)	26. 194	26. 232	26. 227	-0. 019
Roughness (Ra/ $\mu m$ )	0. 46	0. 78	0. 75	0. 29

# Materials Reliability & Mid-term Durability

## Hot corrosion resistance

No weight-loss and strength-reduction were observed even after exposure for 250 hours at 1700°C in addition to 30 wt.% moisture environments.

MGC materials also displayed very superior hot corrosion resistance



Residual 4-point flexural strength after hot corrosion test at 1700°C.



Appearance of the hot corrosion testing equipment



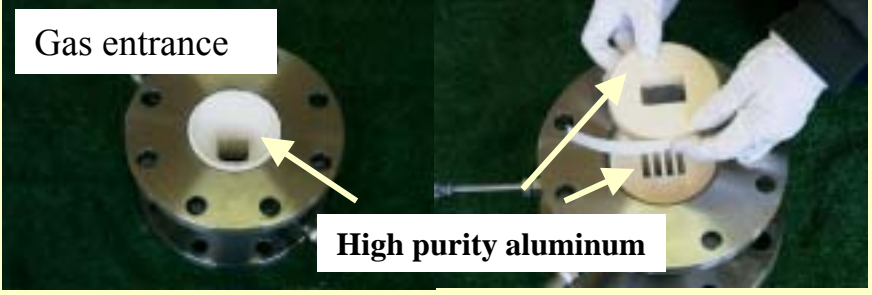
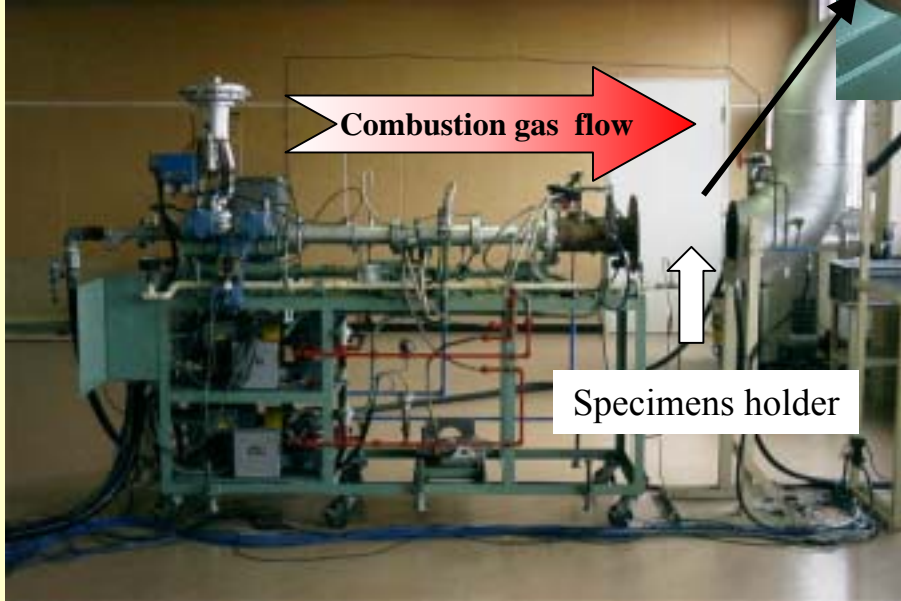
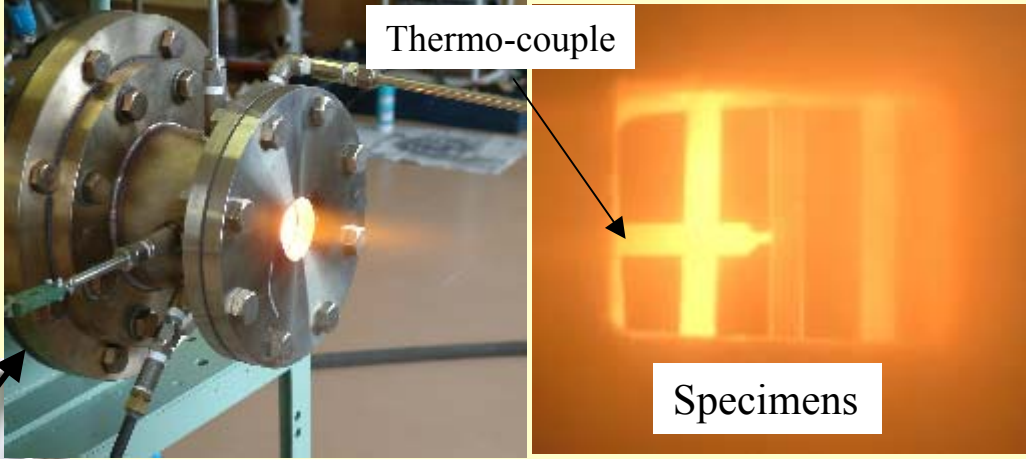
Appearance of the MGC specimens after hot corrosion test

# Exposure tests in combustion gas flow environment

Recently, it has been reported that the recession of conventional ceramics such as  $\text{Si}_3\text{N}_4$ ,  $\text{SiC}$  and  $\text{Al}_2\text{O}_3$ , mainly caused by water vapor is progressing under the combustion gas flow. We have just started exposure tests to evaluate the influence of combustion gas flow environment on MGCs.

### Test machine specification

- \*Fuel : kerosene
- \*Combustion gas exit temperature : 1,600 °C
- \*Combustion gas pressure : 0.3MPa
- \*Combustion gas speed : 500 m/s
- \* Vapor partial pressure : 45KPa
- \*Specimen size : 3\*4\*50 mm



Specimen holder

Appearance of combustion gas flow testing apparatus

# External appearance of the specimens

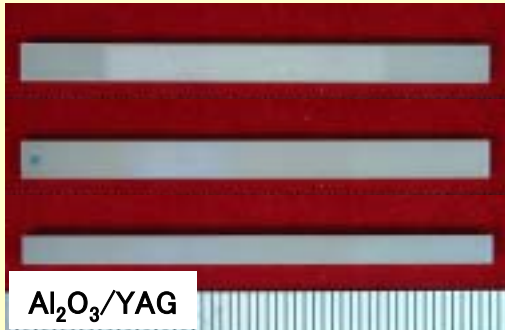
( $T=1,400 - 1,600^{\circ}\text{C}$ ,  $P_{\text{H}_2\text{O}}=15\text{kPa}$ ,  $t=10\text{h}$ )

1,400°C × 10h

1,500°C × 10h

1,600°C × 10h

Upstream

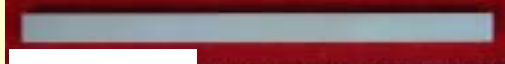


Al<sub>2</sub>O<sub>3</sub>/YAG

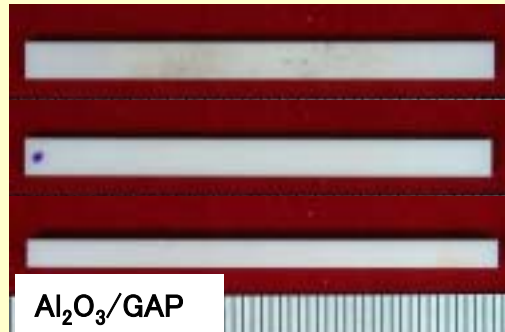
Downstream



Side



Upstream



Al<sub>2</sub>O<sub>3</sub>/GAP

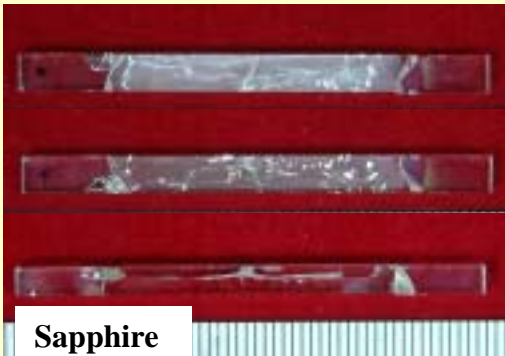
Downstream



Side



Upstream

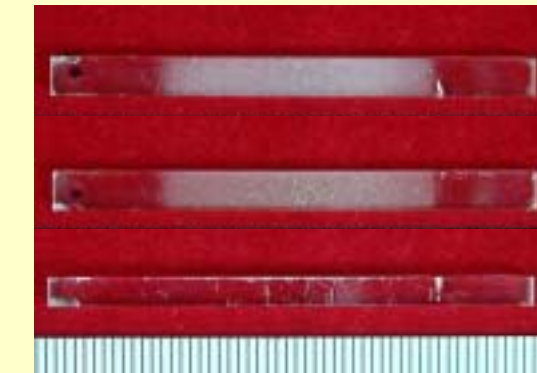


Sapphire

Downstream

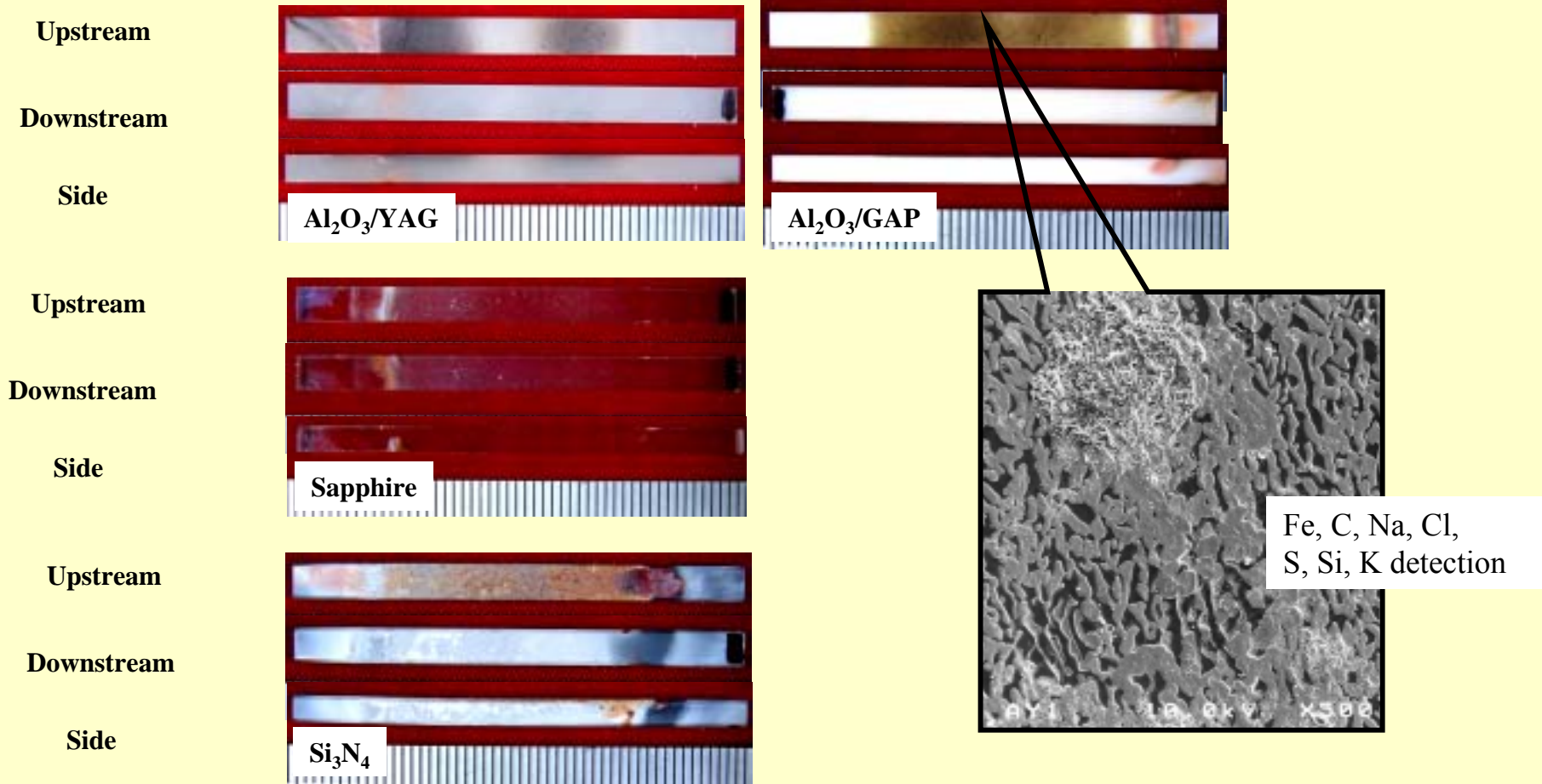


Side





# External appearance of the specimens ( $T=1500^{\circ}\text{C}$ , $P_{\text{H}_2\text{O}}=45\text{kPa}$ , $t=10\text{h}$ )



# External appearance of the specimens

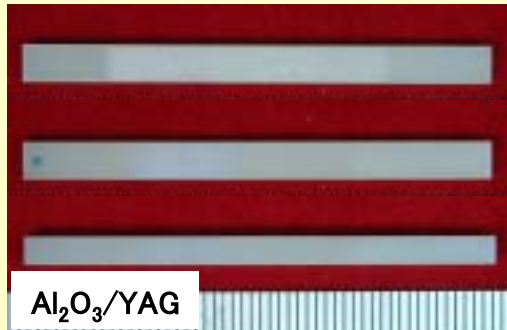
( $T=1,500^{\circ}\text{C}$ ,  $P_{\text{H}_2\text{O}}=15\text{kPa}$ ,  $t= 0 - 25\text{h}$ )

10h

20h

25h

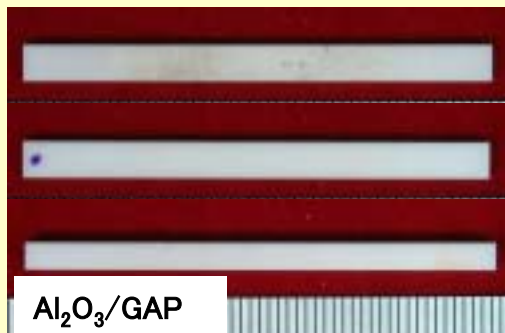
Upstream



Downstream

Side

Upstream



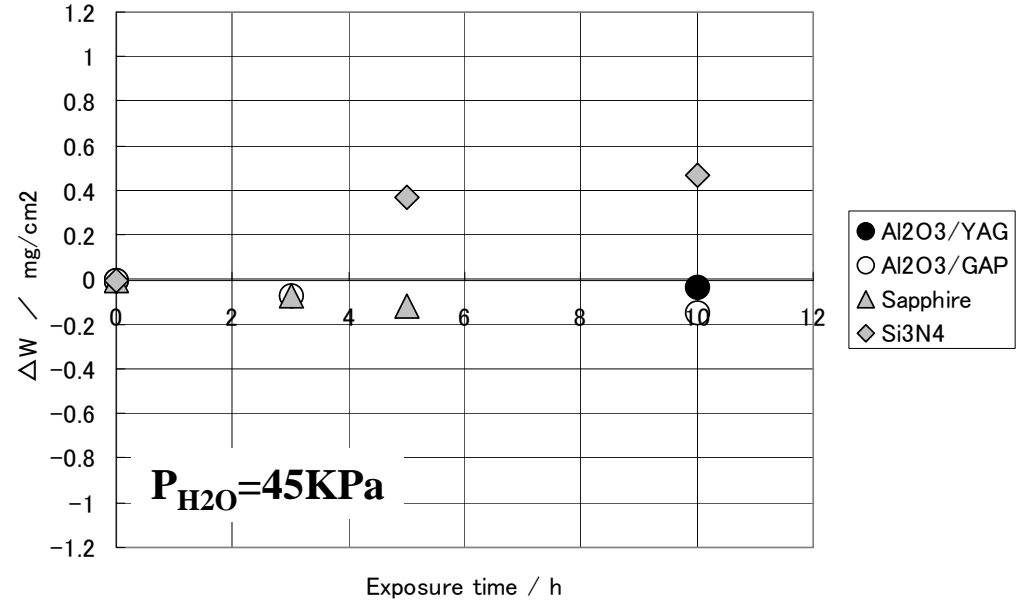
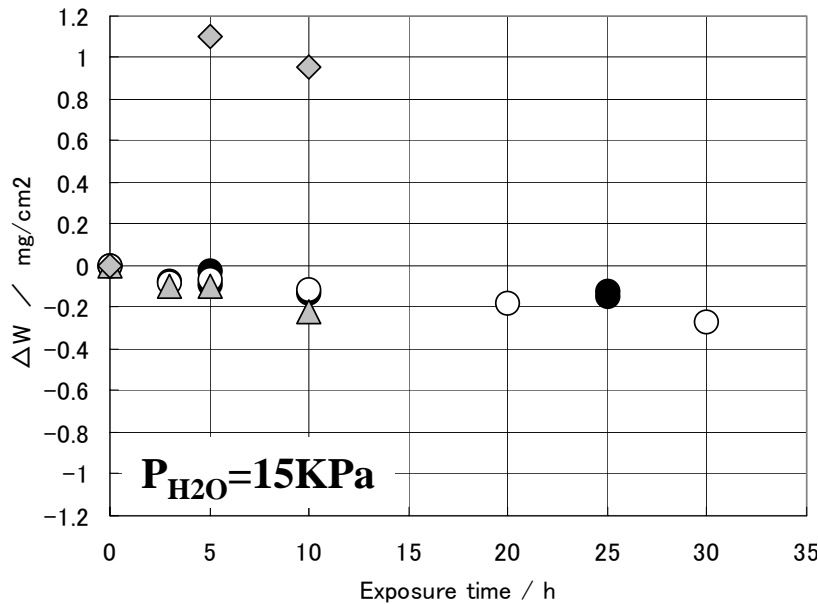
Downstream

Side

Al<sub>2</sub>O<sub>3</sub>/GAP

# Weight change

( $T=1500^{\circ}\text{C}$ ,  $P_{\text{H}_2\text{O}}=15, 45\text{kPa}$ ,  $t=0 - 25\text{h}$  )



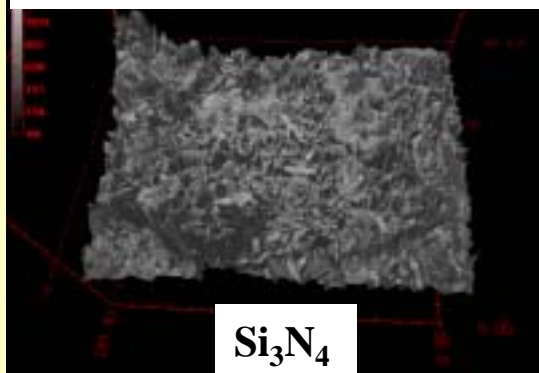
Relationship between exposure time and weight change

Relationship between exposure time and weight change

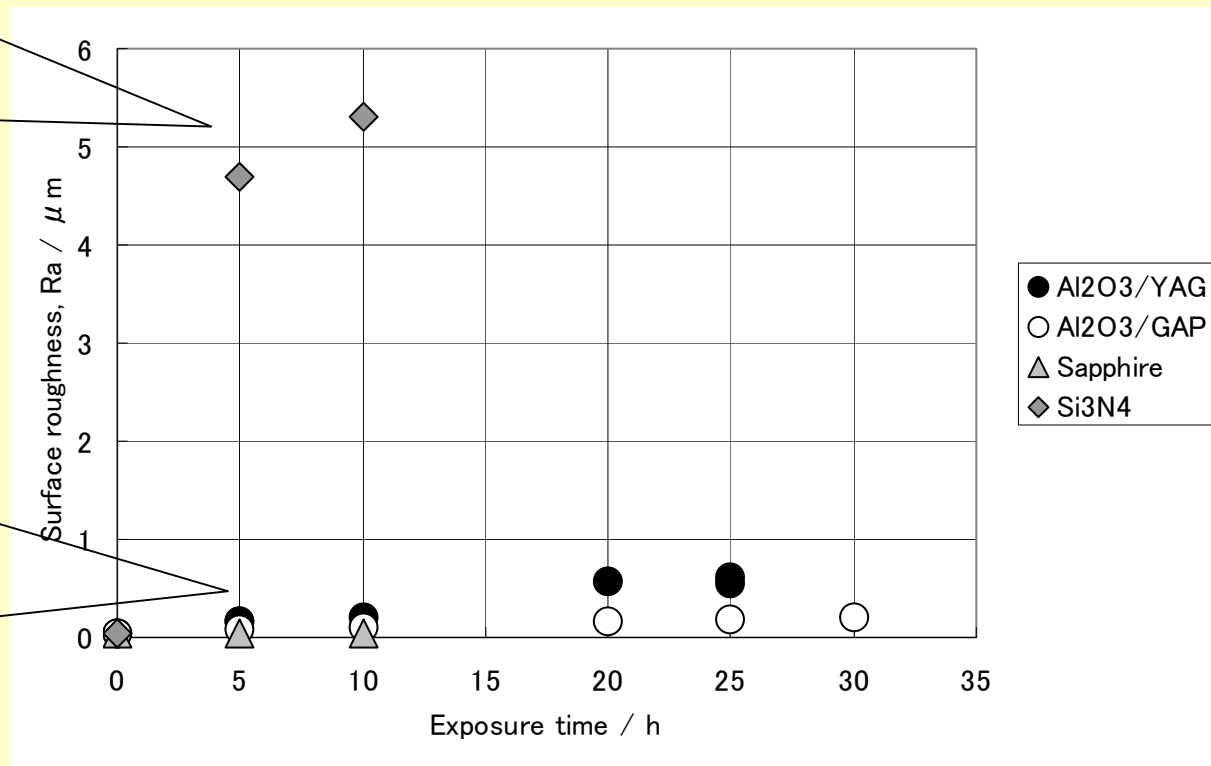
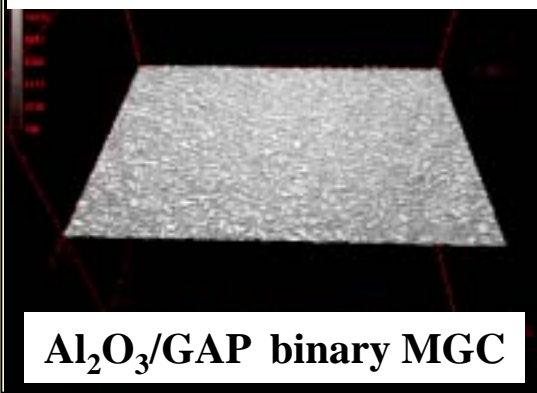
MGC showed  $0.2 \text{ mg/cm}^2$  barely weight loss after 30 hours with the vapor partial pressure of 15KPa. However, the change quantity hardly changes even if vapor partial pressure becomes 45KPa. The weight loss of  $\text{Al}_2\text{O}_3$  single crystal showed  $0.2 \text{ mg/cm}^2$  more than MGCs after 10 hours.  $\text{Si}_3\text{N}_4$  showed  $1.1 \text{ mg/cm}^2$  weight gain after 10 hours with the vapor partial pressure of 15KPa. Furthermore,  $\text{Si}_3\text{N}_4$  showed  $0.5 \text{ mg/cm}^2$  weight gain in 45KPa.

# Surface roughness change of downstream side ( $T=1,500^{\circ}\text{C}$ , $P_{\text{H}_2\text{O}}=15\text{kPa}$ , $t=0-30\text{h}$ )

3D image by Laser microscope

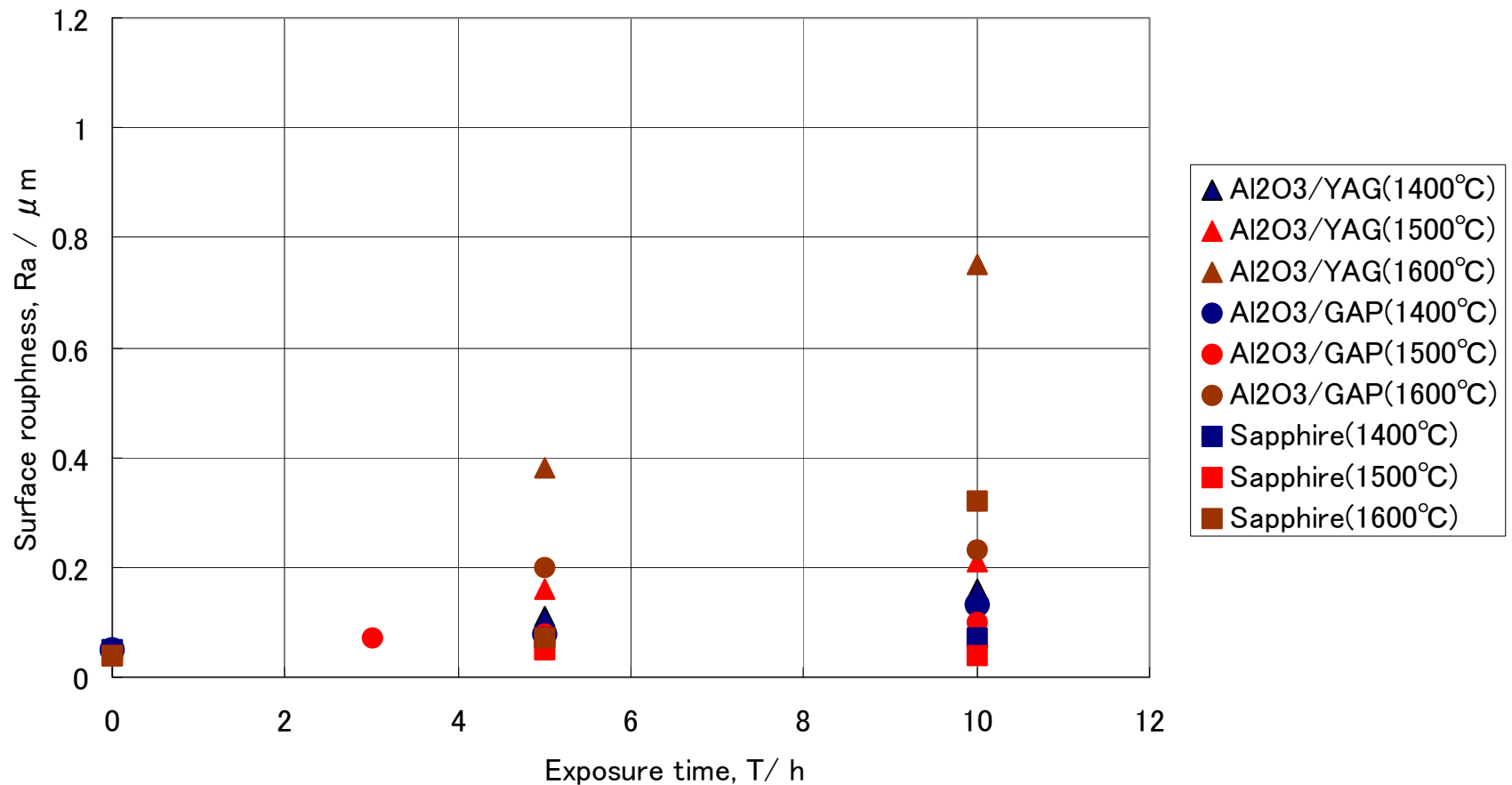


3D image by Laser microscope



MGC and sapphire show the change of the surface roughness like only 0.1- 0.2  $\mu\text{m}$  after exposure test until 30 hours with the vapor partial pressure of 15KPa in combustion gas flow. On the other hand,  $\text{Si}_3\text{N}_4$  shows obvious change of the surface roughness of 5.4  $\mu\text{m}$  after exposure test in 10 hours with the vapor partial pressure of 15KPa. This phenomena is caused by oxidation and scattering of an oxide layers.

# Surface roughness change of downstream side ( $T=1,400 - 1,600^{\circ}\text{C}$ , $P_{\text{H}_2\text{O}}=15\text{kPa}$ , $t=10\text{ h}$ )



Temperature dependence of surface roughness change after the exposure test in combustion gas flow environment at 1400 – 1600 °C.

Al<sub>2</sub>O<sub>3</sub>/GAP binary MGC show the change of the surface roughness like only 0.2  $\mu\text{m}$  after exposure test until 10 hours with the vapor partial pressure of 15KPa in combustion gas flow at 1400 – 1600 °C.

# SEM images of the downstream side surface ( $T=1,400 - 1,600^{\circ}\text{C}$ , $P_{\text{H}_2\text{O}}=15\text{kPa}$ , $t=10\text{h}$ )

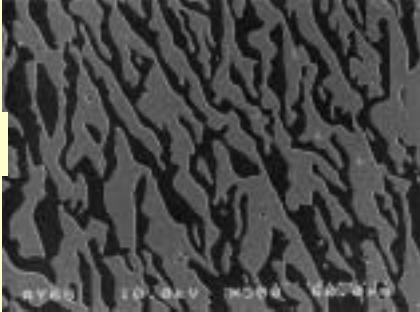
$\text{Al}_2\text{O}_3/\text{YAG}$

$\text{Al}_2\text{O}_3/\text{GAP}$

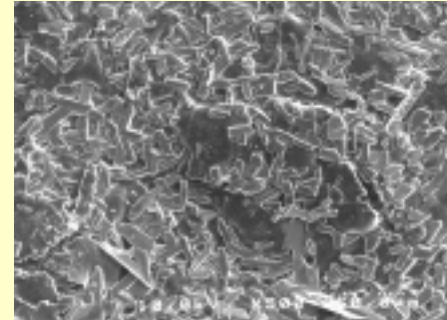
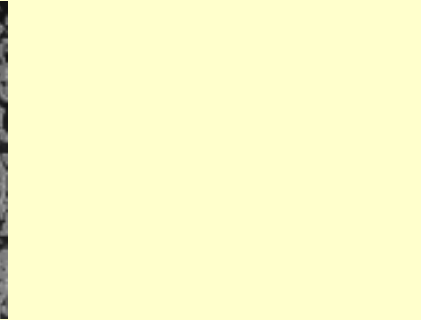
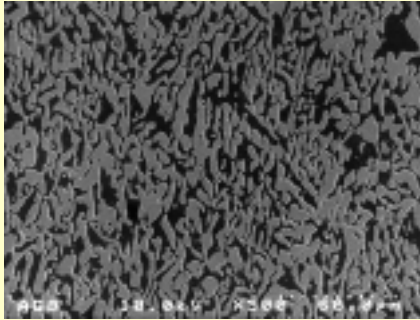
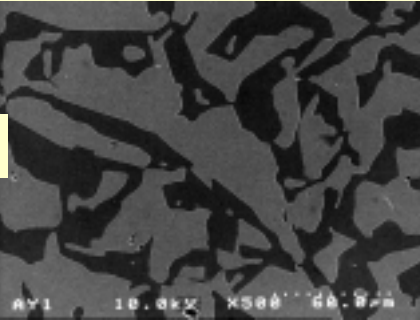
Sapphire

$\text{Si}_3\text{N}_4$

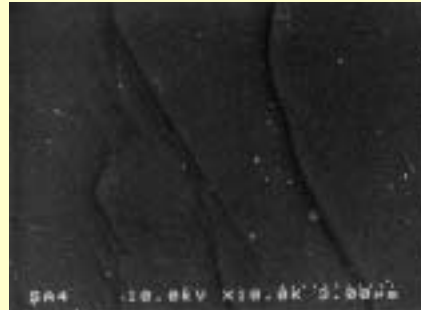
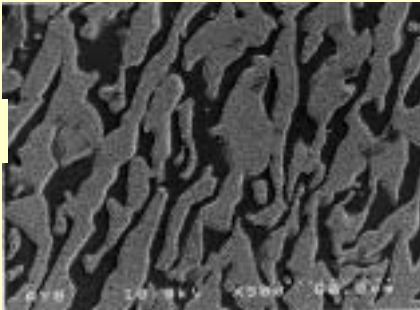
$1,400^{\circ}\text{C}$



$1,500^{\circ}\text{C}$

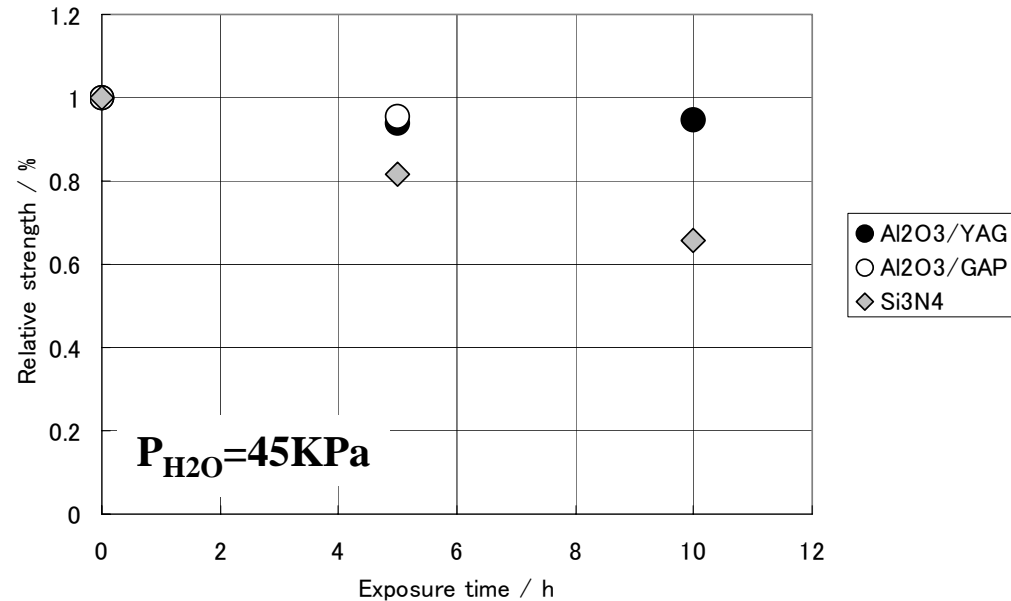
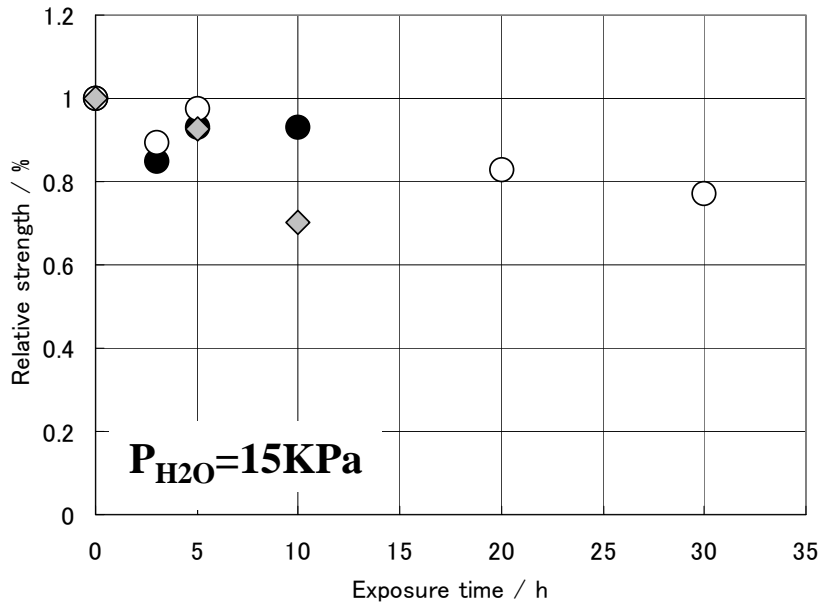


$1,600^{\circ}\text{C}$



# Residual strength

( $T=1500\text{ }^{\circ}\text{C}$ ,  $P_{\text{H}_2\text{O}}=15, 45\text{kPa}$ ,  $t=0 -30\text{h}$ )



Relationship between exposure time and residual strength

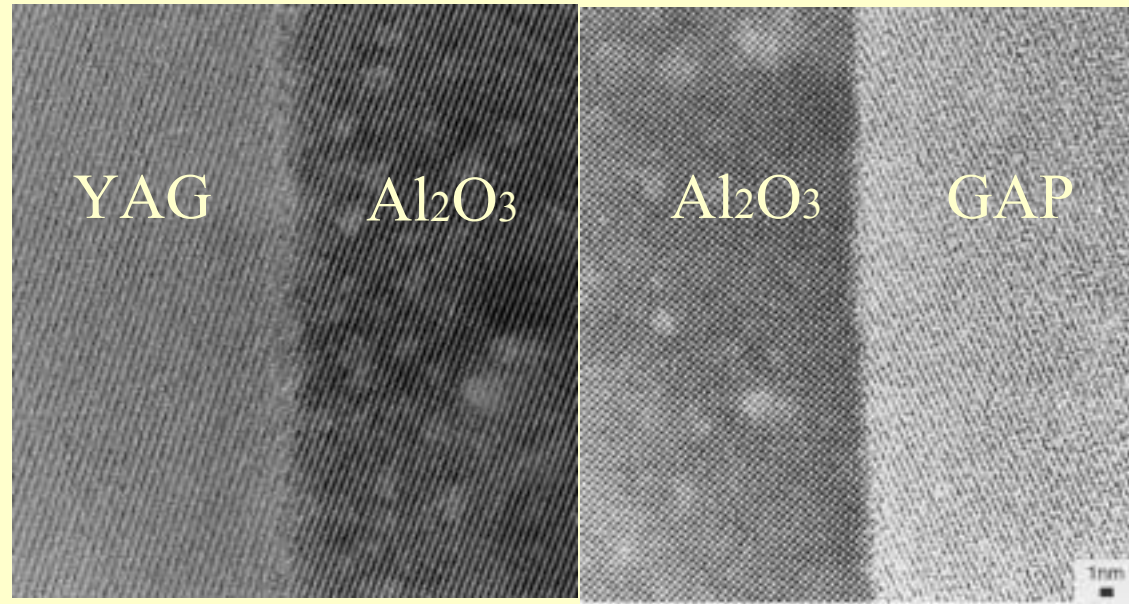
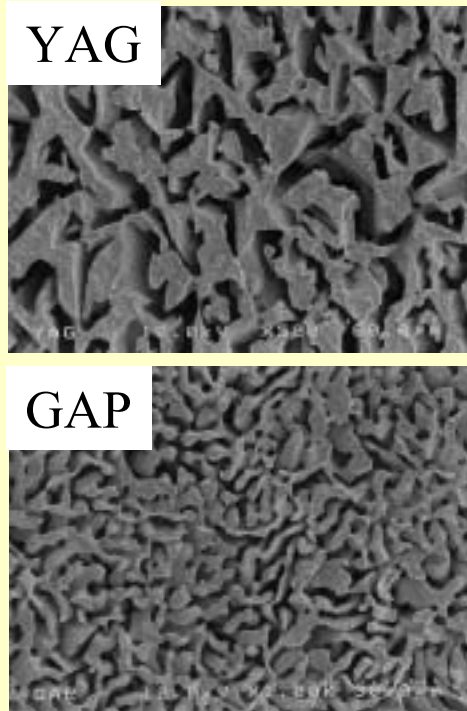
Relationship between exposure time and residual strength

MGC does not show an obvious strength drop after exposure test until 30 hours in combustion gas flow with either vapor partial pressure of 15KPa and 45KPa.

On the other hand, Si<sub>3</sub>N<sub>4</sub> shows 30% of strength drop after exposure test in 10 hours with the vapor partial pressure of 15KPa. Furthermore, Si<sub>3</sub>N<sub>4</sub> shows 35% of strength drop in 45KPa.

# Cause for thermal stabilities characteristics

1. MGC has a microstructure consisting of three-dimensionally continuous and complexly entangled single-crystal  $\text{Al}_2\text{O}_3$  and single-crystal  $\text{Y}_3\text{Al}_5\text{O}_{12}$  or  $\text{GdAlO}_3$ .
2. No amorphous phase were formed at the interfaces between the  $\text{Al}_2\text{O}_3$  and  $\text{Y}_3\text{Al}_5\text{O}_{12}$  or  $\text{GdAlO}_3$  phases.
3. Relatively compatible interface is formed.



These photograph of three-dimensional YAG and GAP phase with only the  $\text{Al}_2\text{O}_3$  phase extruded, after the eutectic composite was heated in graphite powder for one hour at 1600 °C.

High resolution TEM image of the interface between  $\text{Al}_2\text{O}_3$  and  $\text{GdAlO}_3$  phase of the MGC materials.



# Conclusions

---

1. The MGC materials also displayed superior thermal stability of microstructure, strength and oxidation resistance until 1000 hours after heat treatment at 1700 °C in an air.
2. MGC does not show strength drop, weight loss and surface roughening among 10 hours after exposure tests in combustion gas flow environment at 1400 °C.
3. MGC does not show an obvious strength drop, weight loss and surface roughening among 30 hours after exposure tests in combustion gas flow environment at 1500 °C.
4. These excellent high-temperature characteristics are closely linked to such factors as:
  - (1) the composite consisting of a single-crystal  $\text{Al}_2\text{O}_3$  phase and single-crystal YAG or GAP phase with no grain boundaries, no amorphous phase at the interface boundary,
  - (2) the phases being connected three-dimensionally having a complex interlocking structure.

The present MGCs have some advantages as ultra-high temperature structural materials.

The MGCs are expected to be widely used in mechanical engineering at very high temperatures in the future.

# Acknowledgement

---

The authors would like to express their thanks to the New Energy and Industrial Technology Development Organization (NEDO) and the Ministry of Economy, Trade and Industry (METI), who gave them the opportunity to conduct " Research on Technology for MGC Ultra high-Efficiency Gas-turbine System".