# INVESTIGATION OF MICROPOROSITY IN SINGLE-CRYSTAL NICKEL-BASE SUPERALLOYS BY DIFFERENT EXPERIMENTAL TECHNIQUES

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Porosity in single crystal superalloys can be classified into 3 different kinds of pores:

- Solidification: S-pores
- Homogenisation: H-pores
- Creep deformation: D-pores







# Homogenisation $\rightarrow$ H-pores





#### Why is pore characterization important ?



Crack surface with C-pore CMSX-4, LCF, 700 °C,  $\Delta \epsilon$  = 1.2%, R=-1



Dislocations in rafted γ/γ'-structure SRR99, 980°C, 200 MPa, 115 h

- S and H pores are important for the mechanical properties.  $\rightarrow$  Fatigue behaviour.
- D pores are generated during creep.  $\rightarrow$  Deformation mechanism.





# Why is pore characterization difficult ?

• H and D pores are small (about 10  $\mu m$ ).  $\rightarrow$  Difficult preparation.

- Small volume fraction of pores (0.1% $\rightarrow$  0.5%).  $\rightarrow$  High accuracy. (Better than 0.01 absolute %)
- Pores are distributed inhomogeneously.  $\rightarrow$  3D position characterization.
- D pores are not spherical.  $\rightarrow$  3D shape characterization.





#### **Quantitative metallography**

Light microscopy

- •CMSX-4, undeformed
- •14 specimens from one mold

•28 micrographs from each specimen (25,5 mm<sup>2</sup> per specimen)



#### **Density measurements**

When porosity increases density decreases: Methods used:

Gas pycnometery: Helium, 134 MPa, about 10 g superalloy material

Archimedes method: Water or Dodecan, about 200 g superalloy material,

Specimen highly polished:  $\Delta h = \pm 2.5 \,\mu m$ Accuracy of balance: $\Delta m = \pm 0.1 mg$ Stability of temperature: $\Delta T = \pm 1^{\circ}C$ 

 $\frac{\Delta \mathbf{V}}{\mathbf{V}} = -\frac{\Delta \rho}{\rho}$ 











The highest accuracy is attained with

the Archimedes method using water:

Standard deviation of the average density: 3.6 · 10<sup>-5</sup>%





#### Effect of HIP-ing and creep on porosity 0,50 1,2 **Density measurement Creep curve** 0,45 1,0 0,40 vol.% 0,35 0,8 % 0,30 Strain, <sup>6</sup> Porosity, 0,25 0,6 0,20 0,4 0.15 No HIP 0,10 0,2 0,05 HIP 0,0 0.00 900 0 100 200 300 400 500 600 700 800 900 0 100 200 300 400 500 600 700 800 Time, h Time, h CMSX-4, 1100 °C,105 MPa •HIP significantly reduces the porosity of CMSX-4. (After HIP no more pores detectable by LM.) •The increase of porosity at high temperatures and low stresses follows the creep curve.









### Shape of pores



CMSX-4, undeformed



CMSX-4, crept at 1100° C, 117 MPa, 392 h

Pores are round after heat treatment and facetted after creep deformation







#### **Reason for porosity increase**

Superalloy	Mo+Ta+W+ Re [wt%]	Heat treatment		Porosity
		Max. Temp [°C]	Total time [h]	[ /0]
CMSX-6	4,9	1280	10	0.058
SRR99	13,1	1303	5	0.18
CMSX-4	16,5	1303	9	0.20
CMSX-10	20,5	1366	20	0.37

Higher content of refractory element needs a heat treatment with higher temperatures and longer times.









# Shape of creep pores 0.8 µm CMSX-4, 1100°C, 120 MPa, 150 h CMSX-10, 1100°C, 120 MPa, 200 h CMSX-4, 1100°C, 120 MPa, 292 h {100} facets {110} facets **{110} and {100} facets** Creep temperature (1100 °C) is low compared to the homogenisation temperatures (about 1300°C). $\Rightarrow$ Surface energy at creep temperature is anisotropic.



# Summary

•In single crystal superalloys there are 3 classes of pores: Solidification pores, homogenisation pores and creep pores.

•Quantification of porosity by classical metallografy is difficult, because of small pore size, low pore volume fraction and inhomogeneous distribution.

•Differences in porosity can by measured very exactly by the Archimedes method.

•High resolution tomography allows to quantify porosity and to characterize three-dimensionally position and shape of each single pore.

•Pores are concentrated in the interdendritic region.

•Porosity increases with the concentration of refractory elements Mo, Ta, W, Re.

•Porosity increases with creep strain.

•Pore shape transforms during creep from spheres into polyhedrons.



